

Nulling Interferometry

SPIE

March 28, 2000

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JPL

Planet Detection

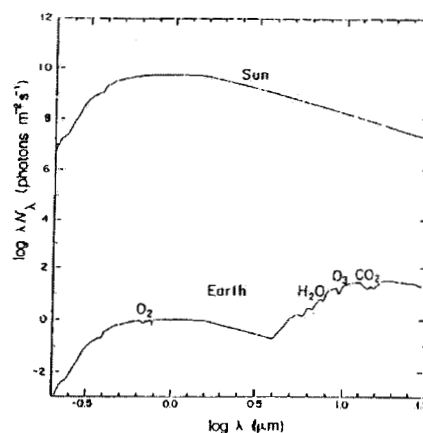
- **Indirect Methods** (= perturbations to stellar parameters):
 - Stellar Position → Astrometry
 - Stellar Velocity → Radial Doppler Shifts
 - Stellar Intensity → Transits, Microlensing
- **Direct Methods** (= direct detection of planetary radiation)
 - Direct Imaging → Very Large Telescopes
 - Starlight Suppression → Coronagraphy,
Nulling Interferometry

Comparison of direct approaches

- 1 AU \Leftrightarrow 1.0 arcsec at 1 pc
0.1 arcsec at 10 pc
- 10-m aperture at $\lambda = 10 \mu\text{m}$ has $\lambda/D = 200 \text{ mas}$
- **To see an exact Earth-analog at 1 AU from its star:**
 - Nulling Interferometry: $\theta < \lambda/D$ ($< \text{few } 0.1 \text{ arcsec}$)
stellar distance $\approx 10 \text{ pc}$
 - Coronagraphy: $\theta > 5 \lambda/D$ ($> 1\text{-}2 \text{ arcsec}$)
stellar distance $\approx 1 \text{ pc}$
 - Direct imaging: $\theta > 10 - 30 \lambda/D$
telescope diameter $> 20 \text{ m}$
- With 10 m or smaller apertures, only nulling interferometry can observe sufficiently close to large numbers of nearby stars in the mid-infrared, where the contrast is reduced.

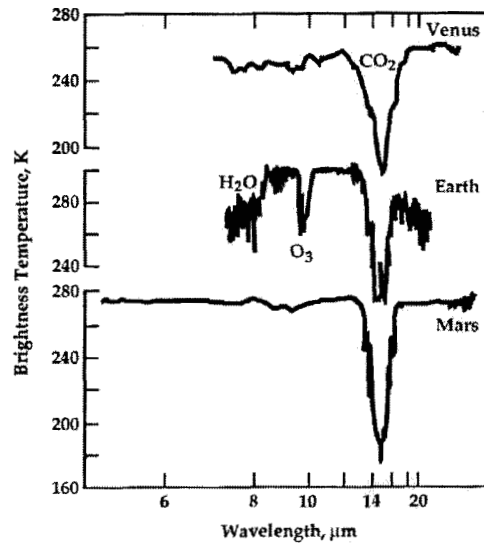
Optimal waveband for direct planet detection

- **Visible Light:**
Reflected Stellar Flux
Contrast = $10^9 - 10^{10}$
- **Thermal Infrared:**
Thermal Planetary Emission
Contrast = $10^6 - 10^7$



Mid-infrared Spectroscopy

- Search for an atmosphere: CO₂
- Search for water
- Search for life
(O₃ in lieu of O₂)



Comparison of MIR Flux Levels

Distance = 10 pc

Wavelength = 10 μm

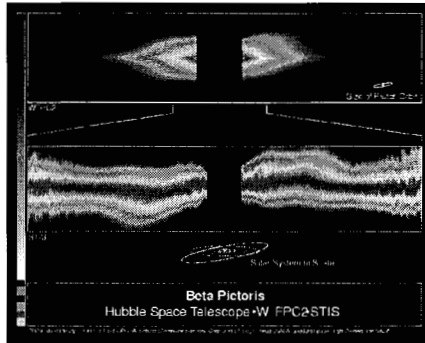
- Signal strengths:

G2 star	2.2 Jy
Exozodiacal emission	200 μJy
Jupiter	2 μJy
Earth	0.3 μJy
- **Solar-level exozodiacal emission**
 is much brighter than planetary emission
- Backgrounds:

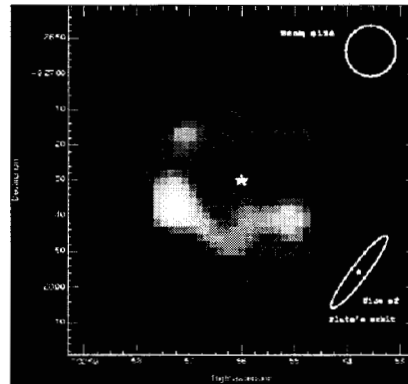
Zodiacal emission	800 μJy
Sky (emissivity = 0.1)	30 Jy

Dust Disks around Nearby Stars

Visible Wavelengths

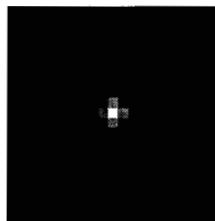


Submillimeter

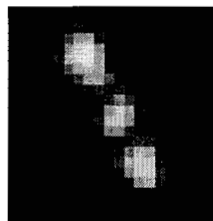


- Both images show dust primarily at > 30 AU
- Cold dust at Kuiper-belt-like radii
- IRAS: 15% of nearby MS stars show cold dust (to limit of 100 zodi)

HR 4796



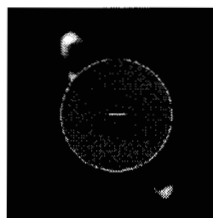
12.5 μm



24.5 μm



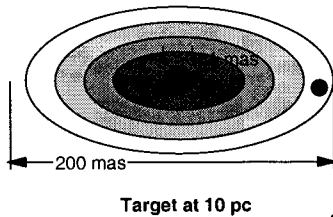
Computer Model



HST/NICMOS

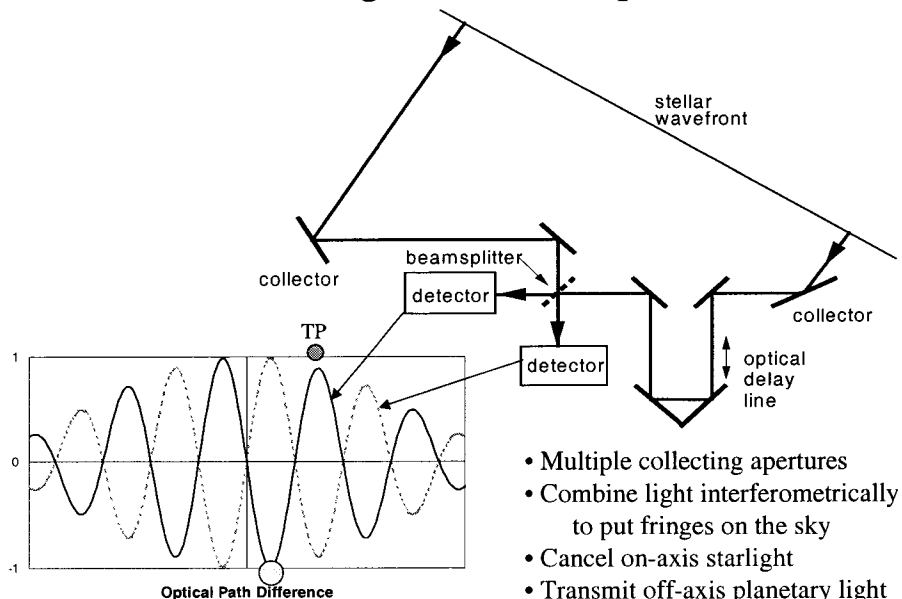
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Nulling Roadmap

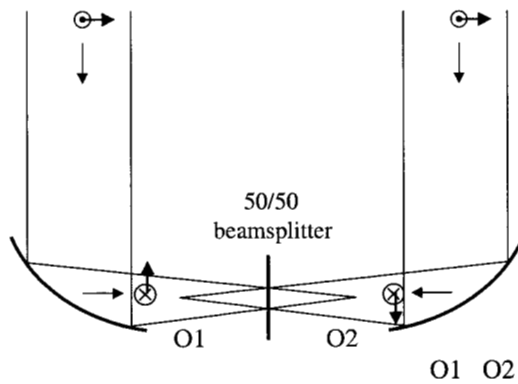


- **Keck:** Characterize exozodiacal MIR emission around nearby stars.
 - Our $10\ \mu\text{m}$ integrated zodiacal flux = 10^{-4} of solar flux
 - 10^{-6} of thermal sky background
 - \Rightarrow Null star **and** remove background.
- **SIM:** demonstrate optical nulling with nanometer-level control needed by TPF.
 - 10^{-6} null @ $10\ \mu\text{m} \Leftrightarrow 10^{-4}$ null @ $1\ \mu\text{m}$
- **TPF:** detect planets at $10\ \mu\text{m}$ in the presence of stellar, zodi, and exozodi fluxes
 - MIR ($7\text{-}20\ \mu\text{m}$) null of 10^{-6} .

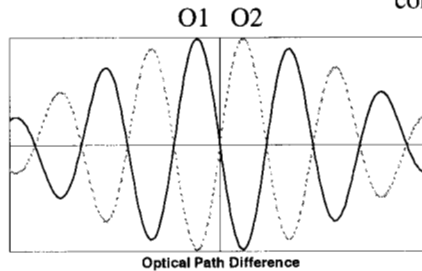
Nulling: Basic Concepts



Original Nulling Concept

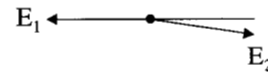


- Symmetric layout: at ZPD
 - ⇒ at ZPD equal (1/2) power to O1 & O2
 - ⇒ complementary fringes at O1 & O2
 - ⇒ no null at ZPD
- Best cancellation at finite OPD
 - ⇒ cancellation is chromatic
- 2 polarizations yield fringes out of phase by π
 - ⇒ fringe patterns cancel completely



General achromatic nulling requirements

- Desire $E_1 - E_2 = 0$
- High degree of **symmetry** and **stability** required:
 - **E** fields in the two input beams oppositely oriented
 - Equal beam intensities
 - Zero relative path difference
 - Simultaneous zero of OPD for both polarizations
 - Simultaneous zero of OPD across aperture:
 - Surfaces typically limit null depth to ≈ 1 - Strehl ratio, or few %
 - ⇒ wavefront cleanup with single mode spatial filter required
 - Simultaneous cancellation at all wavelengths in the passband
 - BW evolution: SIM 20%, Keck 30 - 50%, TPF 100 %
 - Small stellar angular diameter

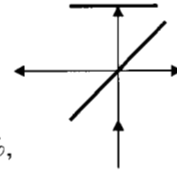


Achromatic Destructive Interference

- Normal “constructive” 2-beam interferometer: $I_{\text{out}} = I_{\text{in}} (1 + V \cos \phi) / 2$

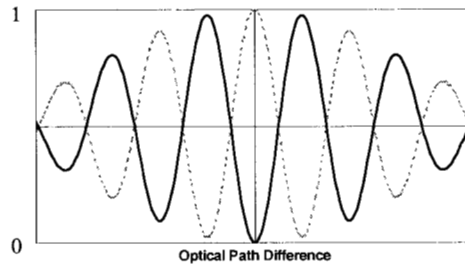
- Bandwidth limitation to destructive interference minima:

$$\frac{I_{\text{min}}}{I_{\text{max}}} = \frac{1}{2} \left(1 - \text{sinc} \frac{\pi \Delta \lambda}{2 \lambda} \right)$$



- For bandwidths of 5, 10, 20, 30, 40, and 50%, the deepest cancellation is 0.05, 0.2, 0.8, 1.8, 3.2, and 5%.

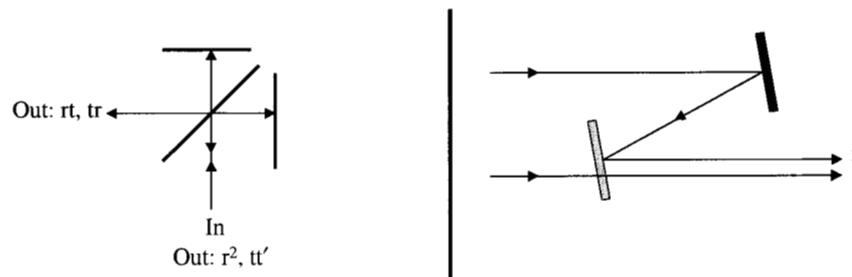
- Deeper cancellation requires an achromatic approach, e.g. a relative field flip:



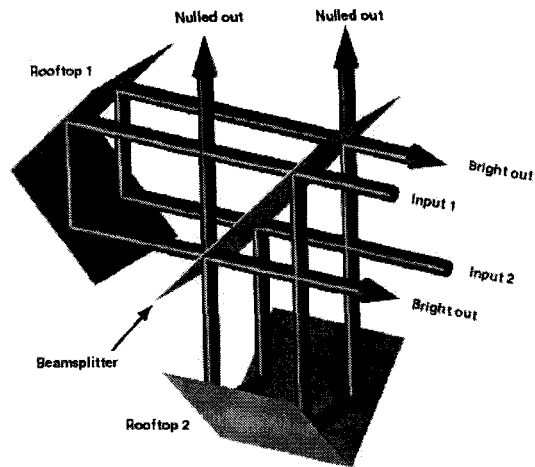
$$I_{\text{out}} = I_{\text{in}} (1 - V \cos \phi) / 2$$

Electric Field Reversal

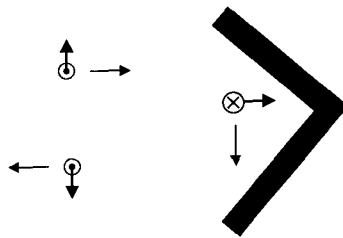
- **Achromatic field reversal can be effected by means of:**
 - Geometric field flip: rotational shearing interferometer
 - Through-focus field flip: (also RSI)
 - Phase retardation: chromatic waveplate



Beam Combination in a Rotational Shearing Interferometer

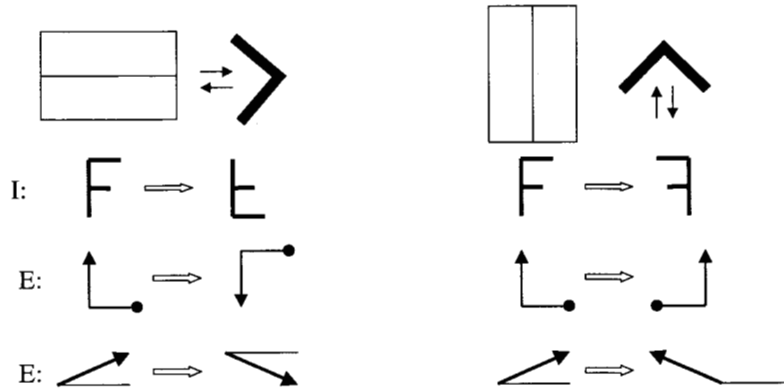


Rooftop Mirrors



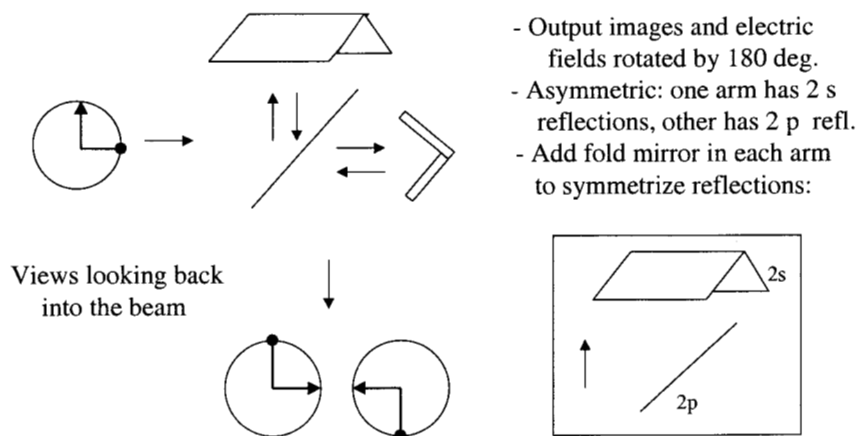
- Rooftop flips E-field component which is normal to roof line

Orthogonal Rooftop Mirrors



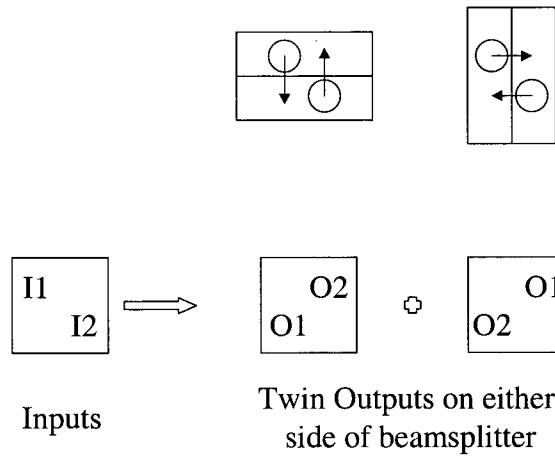
- Electric field vectors orthogonal to rooftop axis flipped by 180 degrees.
- Output beams have polarizations rotated 180 degrees w.r.t. each other.
- Output apertures are rotated 180 deg. w.r.t. each other.

Polarization Compensation

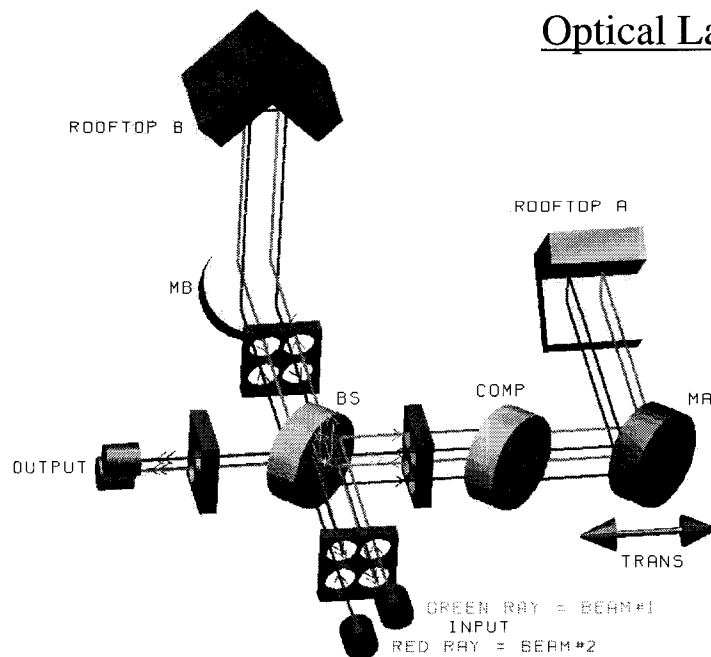


- Output images and electric fields rotated by 180 deg.
- Asymmetric: one arm has 2 s reflections, other has 2 p refl.
- Add fold mirror in each arm to symmetrize reflections:

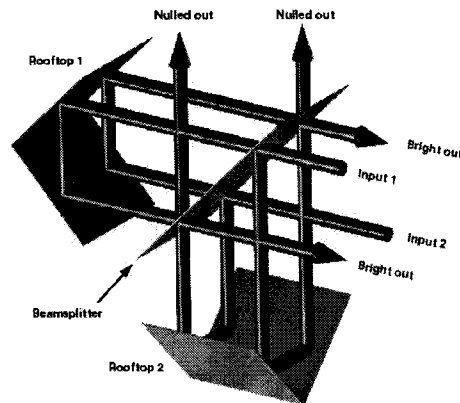
Beam Combination in RSI



Optical Layout



Implementation 1: rotational shearing interferometer



• Advantages:

- Relies solely on flat mirrors
- Achromatic, geometric π phase flip
- Phase flip separated from OPD
- Nearly perfect symmetry (with extra folds)
- Automatic power balance:
Beamsplitter used in double-pass, so same RT product multiplies both inputs
- High R/T ratio tolerance at 2-pass b.s.
(R near 0.5 only maximizes throughput)

• Drawbacks:

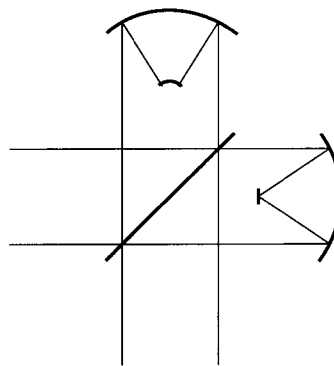
- High quality rooftop reflectors needed

• Both:

- 2 nulled outputs

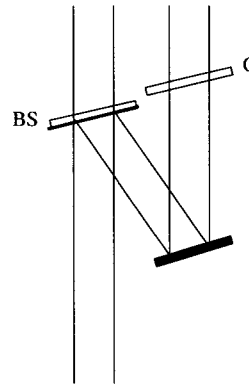
Implementation 2: Phase shift through focus

- Passing through focus inverts aperture, adds achromatic 180 degree phase shift.
- Replace rooftops by cat's eyes:
 - one secondary flat, at focus
 - other secondary curved, prior to focus
- Advantages:
 - Achromatic 180 degree phase flip
 - Phase flip separated from OPD
 - Relaxed b.s. R/T requirements
- Disadvantages:
 - Differing angles of incidence on secs.
 - Point focus on flat secondary
 - 2 nulled outputs



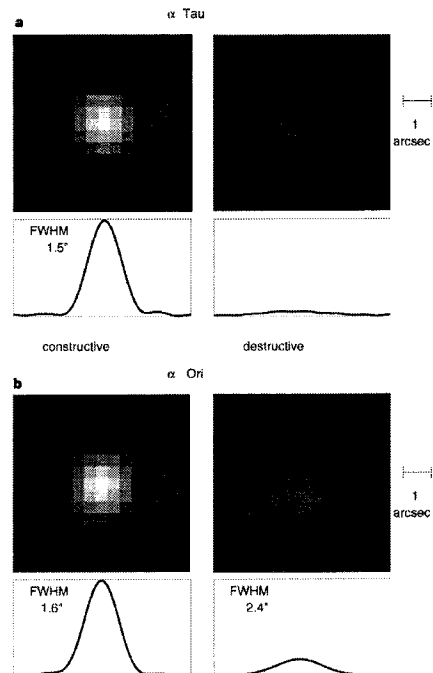
Implementation 3: dielectric waveplate

- 90 degree phase shift at b.s.
- Dielectric plate compensates for b.s. plate;
adds another 90 degree phase shift.
- **Advantages:**
 - simple layout and components
 - no wavefront inversion
 - one nulling output
 - can use a second waveband to sense OPD
- **Challenges:**
 - Requires highly accurate coatings:
single-pass beamsplitter requires nearly
perfect R/T match for intensity balance
 - Requires highly accurate tailoring of
compensator refractive indices across band.
 - Phase flip and OPD not independent.



UofA MMT MIR nulling

- Waveplate scheme
- On telescope
- Cancelled 2 panels of MMT
- Rejection of 1/24 achieved
- No OPD control



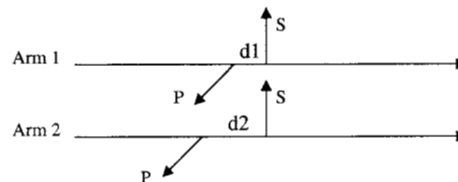
Wavefront Cleanup

- Aberrated wavefronts prohibit simultaneous field cancellation across the wavefront. N limited to about 1-S.
- Wavefront cleanup required for deep nulls
- Effected by means of a spatial filter in output focal plane
- Only the point-spread function core is transmitted
- Limits nulling to a single spatial mode of the telescope



Sources of null degradation

- | | |
|--|-------------|
| • Finite Stellar Diameter | Static |
| • Nonunity visibility: | |
| - Wavefront errors - removed by spatial filtering | Static |
| - Polarization rotation mismatch | Static |
| - Intensity mismatch: transmission asymmetries, | Static |
| pointing jitter induced scintillations | Fluctuating |
| • Nonzero phase: | |
| - Optical path jitter | Fluctuating |
| - Differential s-p polarization delay (d_1 - d_2 below) | Static |
| • Dispersion | Static |



Null Depth Definition

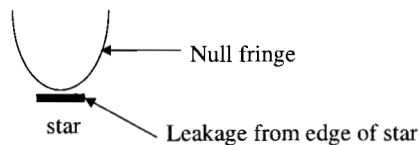
- Null depth : $N \equiv I_{\min} / I_{\max}$
 where I_{out} and I_{in} are the nuller throughputs in the destructive and constructive states, respectively.

$$N = (1 - V \cos \phi) / 2.$$
- Both $V < 1$ and $\phi \neq 0$ limit null depth and so drive the requirements.
- For $V=1$ and small phase errors $N = (\phi / 2)^2 = (\pi x / \lambda)^2$
- For perfect phase matching $N = (1 - V) / 2.$
- Examples:
 For $N = 10^{-4}$, $V = 0.9998$.
 For $N = 3 \times 10^{-5}$, $\lambda = 600 \text{ nm}$, $x = 1 \text{ nm}$
 For $N = 3 \times 10^{-5}$, $\lambda = 10 \text{ }\mu\text{m}$, $x = 17 \text{ nm}$

How deep is your null?

- Fundamental limit: Nonzero stellar diameter limits N to:

$$N = \frac{\pi^2}{16} \left(\frac{\theta_{\text{dia}}}{\lambda / b} \right)^2$$



- For a G2 star @ 10 pc, with an angular diameter of 0.93 mas, $N=3\text{e-}5$ at $0.63 \text{ }\mu\text{m}$ requires a projected baseline of $< 1.0 \text{ m}$.
- Note: A flux reduction by 10^{-4} corresponds to 10 magnitudes:
 On SIM, this leaves a flux of order 1000 photons/s/aperture.

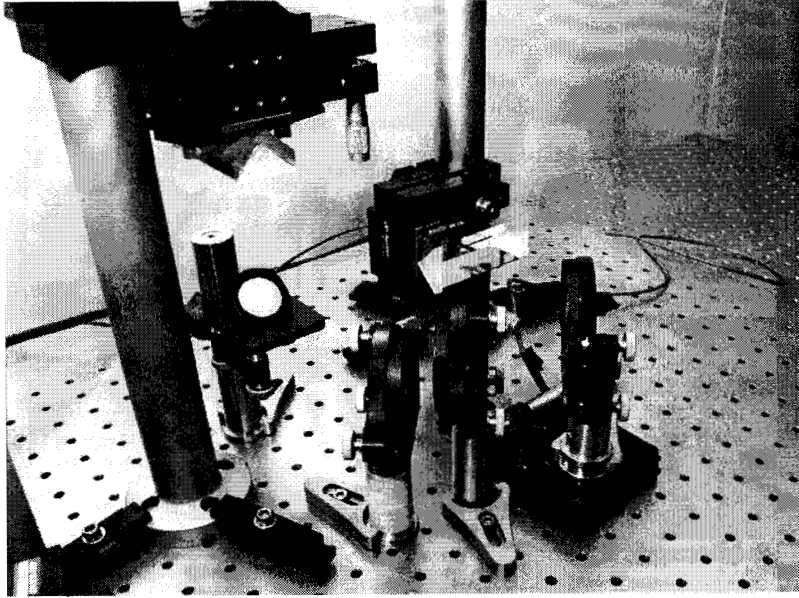
SIM requirements from null depth

	Constraint	Null Contribution	Requirement	
Stellar Diameter Leakage	$\theta_{\text{dia}} < 4\lambda\sqrt{N}/\pi b$	$< 3\text{e-}5$	$b < 1.1 \text{ m}$	
Optical Path Errors	$x < \lambda\sqrt{N}/\pi\sqrt{1+\sqrt{2}}$	$< 3\text{e-}5$	$< 0.8 \text{ nm}$	
Transmission Asymmetries	$\Delta/I < 4\sqrt{N}$	$< 1\text{e-}5$	$< 1.2 \%$	
Pointing Jitter	$\alpha < 0.8(\lambda/D)^{4/3}\sqrt{N}$	$< 1\text{e-}5$	25 mas	$\frac{1}{22} \frac{\lambda}{D}$
Differential Polz'n Rotation	$\phi < 2\sqrt{N}$	$< 1\text{e-}5$	$< 0.36 \text{ deg.}$	
Differential s-p Polar. Delay	$\Delta < 4\sqrt{N}$	$< 1\text{e-}5$	$< 0.72 \text{ deg.}$	

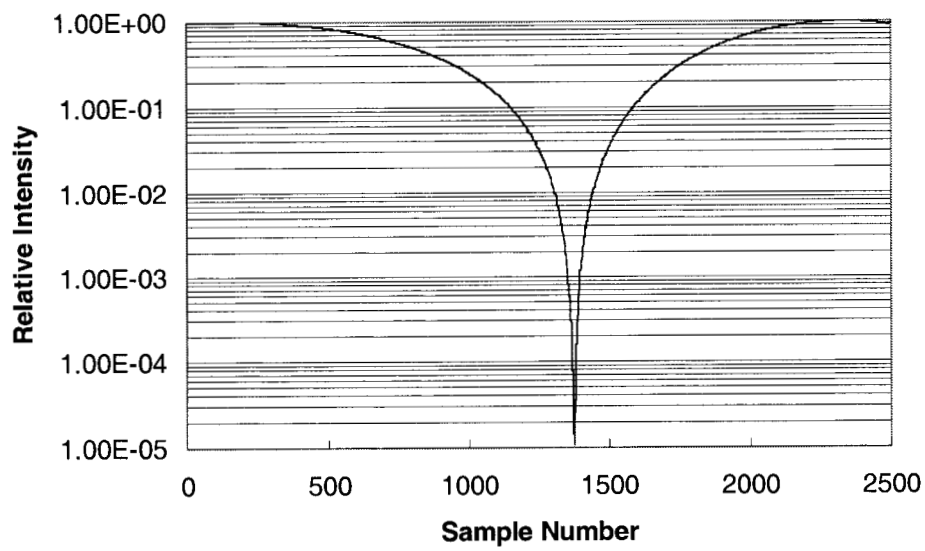
Keck requirements from null depth

	Constraint	N=1e-4 Req.	N=1e-5 Goal	Impactee
Differential Image Rotation	$\theta < 2\sqrt{N}$	< 1.1	< 0.36	LDL
Throughput Asymmetries	$\frac{I_{\text{diff}}}{I} < 4\sqrt{N}$	$< 4\%$	$< 1.2\%$	Coatings
Strehl Fluctuations (1-S)	$\frac{\sigma_I}{I} < 2\sqrt{N}$	$< 2\%$	$< 0.6 \%$	AO
Optical Path Errors	$x < \frac{\lambda}{\pi}\sqrt{N}$	$< 32 \text{ nm}$	$< 10 \text{ nm}$	FDL
Feed Forward Time	$\frac{t_{\text{ff}}}{t_{02}} < (2\sqrt{N})^{6/5}$	$< 0.7 \text{ msec}$	$< 0.18 \text{ msec}$	Frng Trckr
Differential s-p Polar. Delay	$\Delta < 4\sqrt{N}$	< 2.3	< 0.72	Coatings

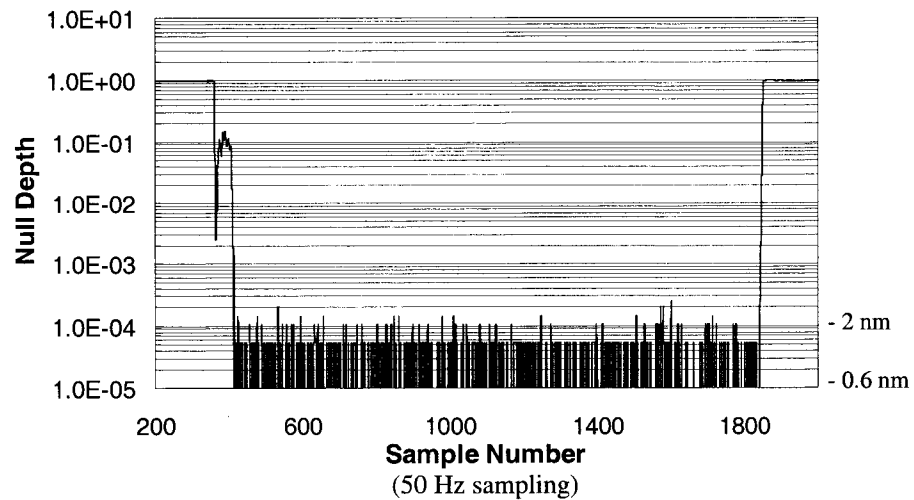
Experimental Setup



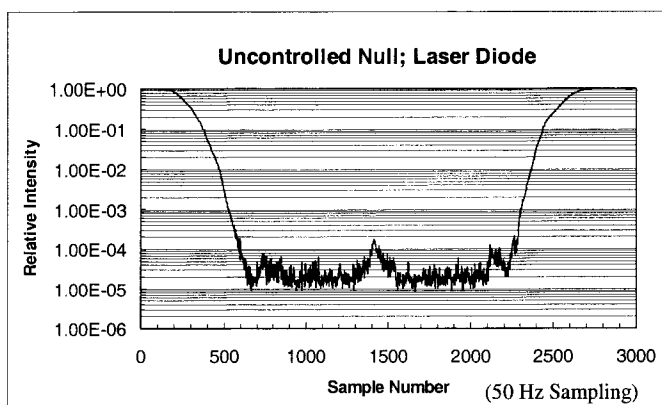
Laser Diode OPD Scan



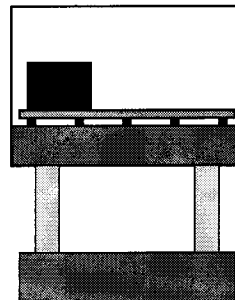
Dither-controlled Laser Null

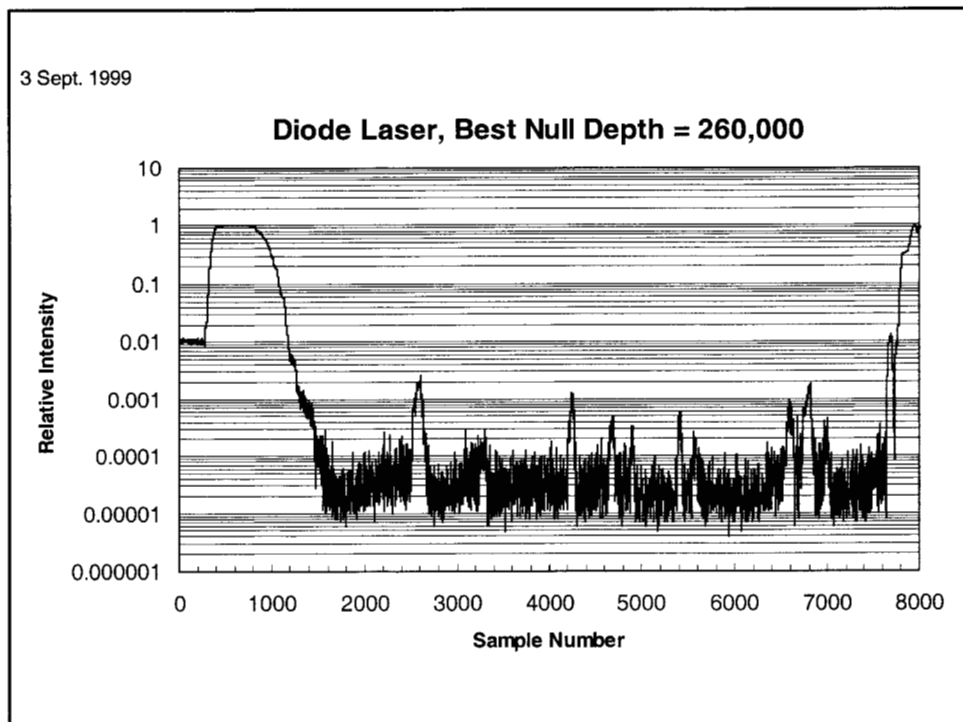
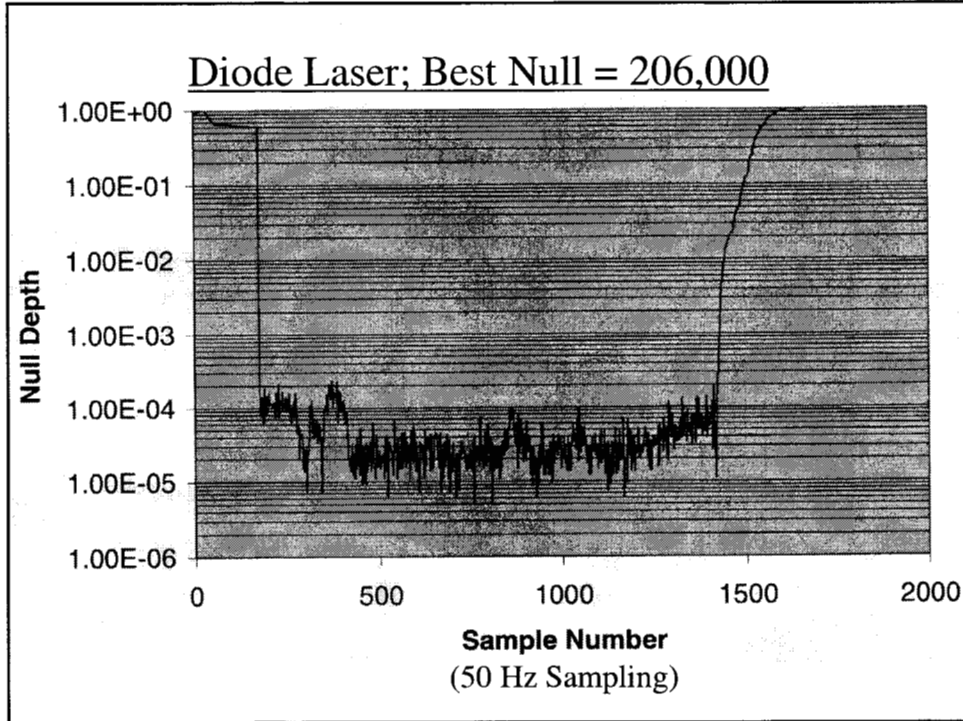


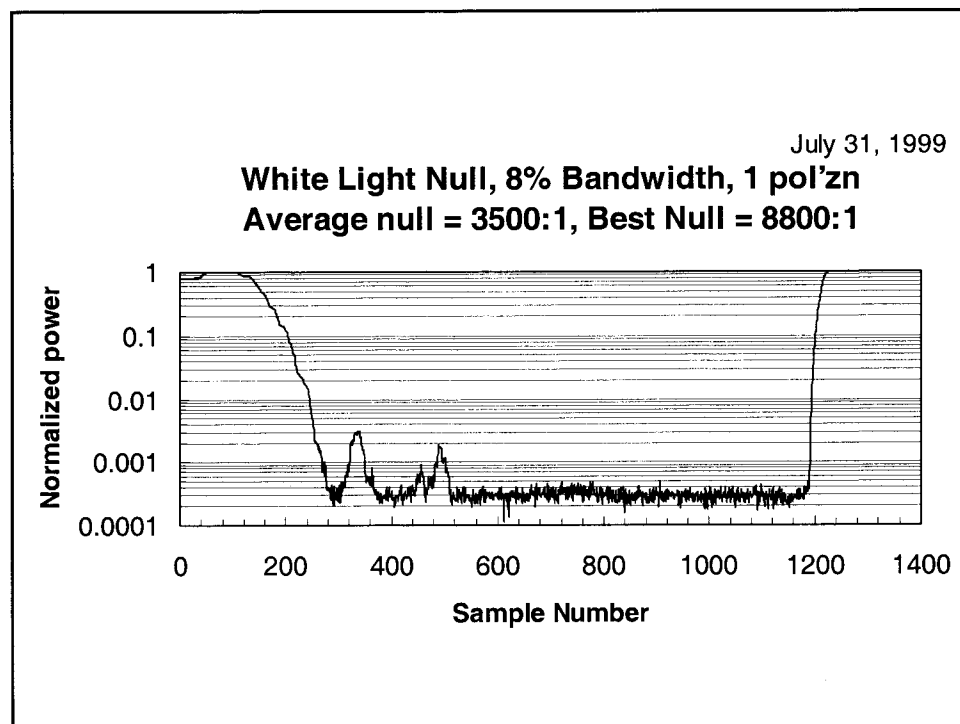
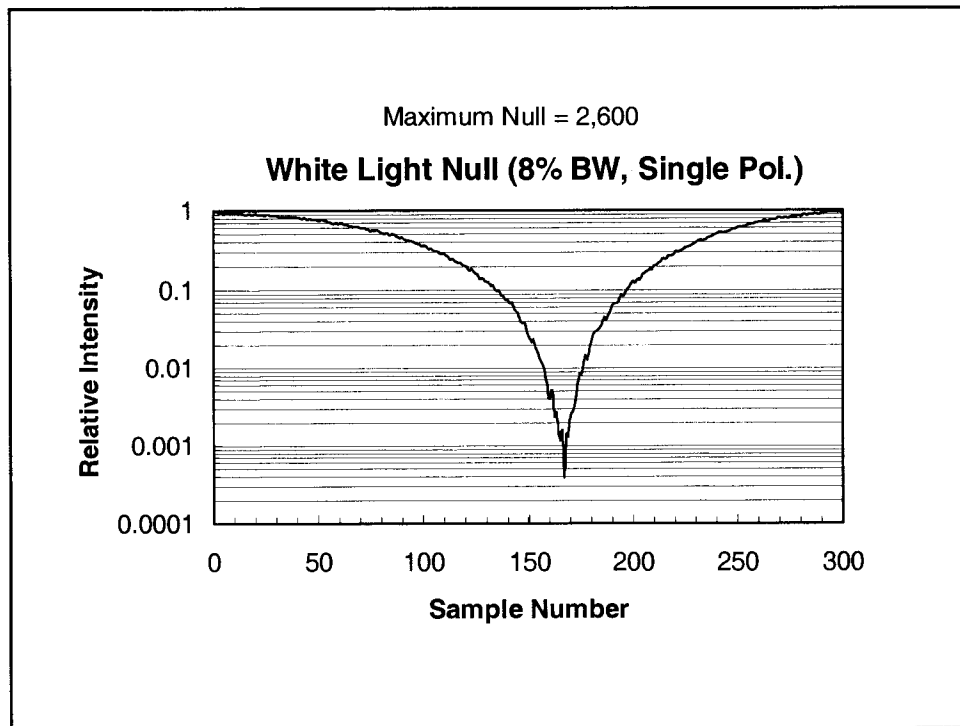
Environmental Improvements in New Lab:

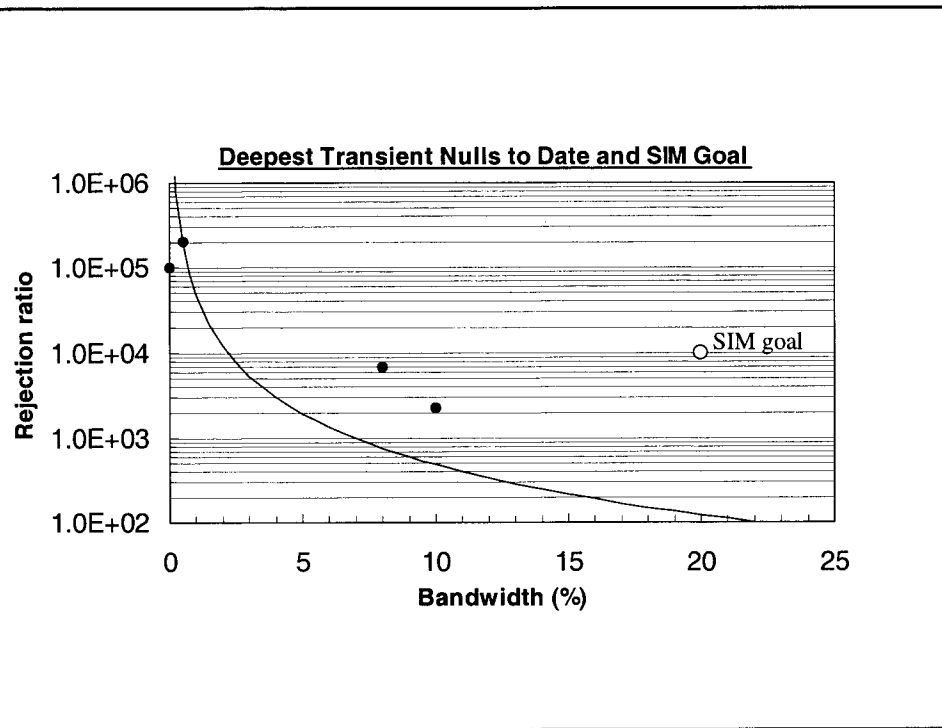


Vibration and
Acoustic Isolation









Sources of null degradation for wider bands

- Input lens decenter
- Input polarizer wedge angle
- Beamsplitter/compensator thickness or rotation mismatch
- Beamsplitter/AR coating phase shifts
- Unequal number of AR coating traversals (BS/Comp)
- Mirror protective coating asymmetry
- Extra reflections in filters, polarizers
- Intensity balance vs. wavelength

The Future: Control and Modulation Schemes

- Active Intensity Matching
- OPD Control:
 - Control one output by means of the second
 - Control one waveband by means of another
 - Control via metrology
- Signal Modulation Schemes:
 - Baseline rotation: fringes sweep across zodi/planet
 - Spatial chopping:
 - nulling removes star; chop on/off zodi/planet
 - OPD fringe scan after multiple baseline nulling

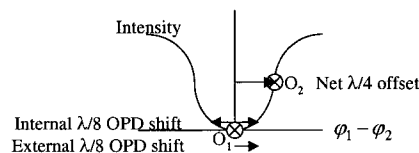
Intensity Matching

- Intensities in the two beams must be matched achromatically;
 - dielectric attenuators are excluded.
- Pointing and beam vignetting both affect intensity;
 - desirable to divorce pointing from intensity control (to the extent possible).
- Employ both beam vignetting and pointing to modify intensities:
 - Rooftop tilt actuator used for fine pointing/intensity control.
 - Modulate flux via rotating ``Venetian blind'' across aperture center.
 - Use variably shadowed obscuration, i.e., ``scissors''.



Optical OPD control

- **Approach:** The nuller has 2 outputs. Use 1 output to control the 2nd.
- **How?**
 - An *internal* nuller path delay causes the two nuller outputs to depart from null in opposite directions (opposite relative phases):
Output 1 has E_1 ahead of E_2 ; output 2 has E_2 ahead of E_1 .
 - An *external* path delay (i.e., prior to the nulling combiner) *always* advances one beam relative to the other.
- \therefore The 2 types of offsets can be combined to leave one nuller output on null, and the second output at an OPD offset of $\lambda/4$.
- At the quadrature output, a large signal and a linear intensity-OPD relation are available for control. Control sensitivity at half-power output:



$$\frac{\Delta I}{I} = 2\pi \frac{\Delta x_{\text{OPD}}}{\lambda}$$

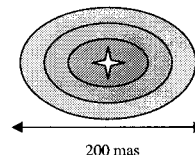
or $\approx 1\%/nm$

Keck Nulling Science Objectives

- Non-stellar MIR emission from nearby solar systems likely to be dominated by thermal exozodiacal emission from dusty disks, making planetary thermal emission difficult to detect.
- Prior to TPF, first probe exozodiacal flux levels around nearby stars with Keck-Keck single-baseline interferometry.
- Zodiacal/Stellar flux ratio @ 10 microns for our sun $\approx 1e-4$.
- The 85 m K1-K2 baseline can characterize exozodi emission on sub-AU scales.

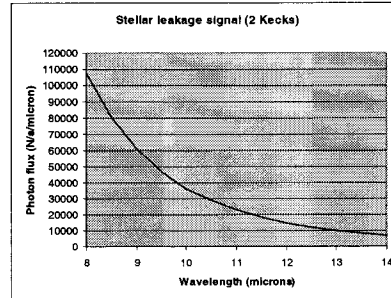
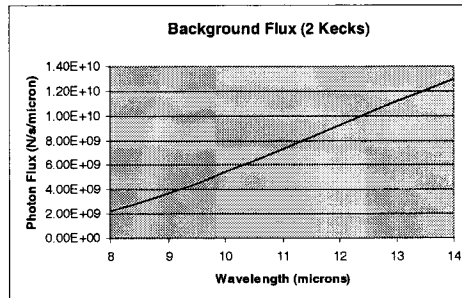
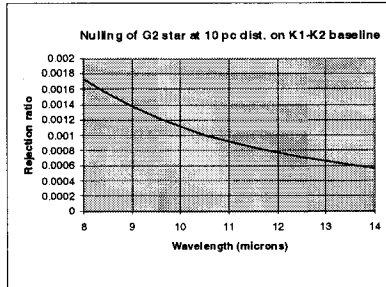
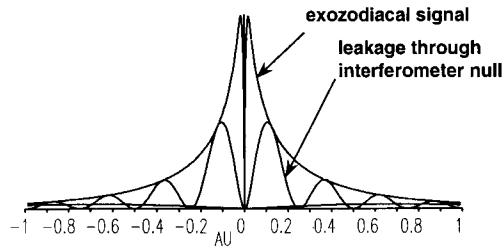
Angular sizes:

G-star diameter at 10 pc:	1 mas
1 AU at 10 pc:	100 mas
K1-K2 10 μ fringe spacing:	24 mas
Keck 10 μ beam diameter:	200 mas

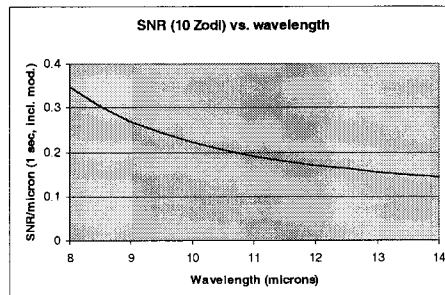
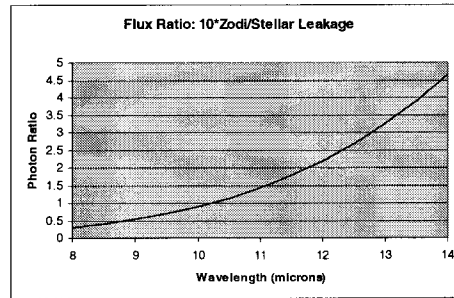
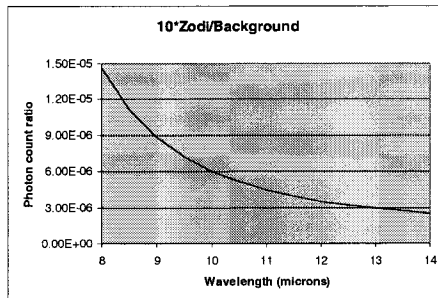


- Requirement: detection capability at the 10-solar-zodi equivalent
- Goal: 1-solar-zodi equivalent

Signals: I



Signals: II



SNR for exozodiacal signal at Keck

- Pessimistic case: $\lambda = 10 \mu\text{m}$, $\Delta\lambda/\lambda = 0.3$, emissivity = 0.65, total system efficiency = 0.046, cold throughput = 0.14, $A\Omega = \lambda^2$, 9 m diameter
- **Detection rates:**
 - G star at 10 pc (2 Kecks) = $9\text{e}7$ photons/s
 - Stellar leakage thru null = $9\text{e}4$ photons/s
 - 10 solar zodi (2 Kecks) = $8\text{e}4$ photons/s
 - Background (2 Kecks) = $1.8\text{e}10$ photons/s
 - Noise (1 sec) = $1.35\text{e}5$ photons
 - SNR (1 sec; 10 solar Zodi; including modulation) = 0.2
 - SNR (4 hr; 10 solar Zodi; including modulation) = 25

Future Work

- Broaden Bandwidth
- Move into Mid-Infrared (Cryogenic)
- Dual-polarization Nulling
- White-light Null stabilization
- Efficiency optimization
- Control architectures
- Component development (rooftops, beamsplitters, single-mode filters, AR coatings, etc.)
- Null at high altitude
- Null in space